

## IntegraLine" ${ }^{\text {" }}$

Corrosion/Abrasion-Resistant FRP Pipe For Power Plants


## Introducing IntegraLine* Pipe

After years of serving corrosion-related industries, Fibrex noticed there seemed to be no easy approach to selecting and designing fiberglass reinforced plastic (FRP) pipe. Most plants have worked with fabricators and engineers to custom design all FRP equipment. Yet there is considerable cost and effort to custom design pipe or a pipe system and it is not always necessary. Fibrex has found there are many applications where a standard FRP pipe product will meet all of the requirements. That's why Fibrex has developed a standard pipe product line called IntegraLine.

IntegraLine is a standard production pipe with custom corrosion resistance. Simple to specify and select, this pipe is ideal for new system installation or replacement of existing pipe. IntegraLine pipe will meet many of the applications and life-span requirements at your plant or facility.

IntegraLine AR combines the corrosion resistance characteristics and construction features of IntegraLine chemical pipe with the added attribute of abrasion resistance. IntegraLine AR can be provided with an abrasion barrier on both the interior and exterior of the pipe where required.

For special design requirements, Fibrex also offers custom-pipe solutions. Custom-pipe solutions may require thicker corrosion or abrasion barriers with different resins. Also, heavier structural laminates and special glass reinforcements are available to meet installation and temperature requirements. Fibrex can provide design recommendations for a proposed installation.

And because Fibrex understands the industries we serve, Fibrex products are designed to meet the most demanding and specialized conditions at each site. In standard pipe, custom pipe, special header systems, duct or stacks, Fibrex delivers long-term corrosion solutions and absolute maximum product life. We call this "performance-based manufacturing."

- cost savings
- faster production and quicker delivery
- fast and easy pipe selection

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## Corrosion Resistance

IntegraLine FRP pipe is designed to provide consistent corrosion resistance for the majority of chemical applications for which FRP pipe is considered appropriate. There remain certain extreme chemical applications for which special construction and/or alternative resins should be considered. These are noted in the chemical resistance guides of the resin manufacturers, available from Fibrex. The use of special construction features, such as thicker corrosion barriers, will change some of the dimensional data in this manual.

> Abrasion Resistance
> IntegraLine AR abrasion-resistant pipe utilizes a granular ceramic in the corrosion barrier to produce an extremely hard surface that resists erosion by abrasive slurries. For applications in which the pipe may be exposed to exterior forces of erosion, such as FGD scrubbers, the pipe will have an abrasion-resistant barrier on the exterior of the pipe as well as the interior. The exterior abrasion-resistant layer may utilize alternative materials as deemed appropriate for the service. Note that application of an exterior abrasion barrier will increase the total wall thickness and outside diameter of the pipe.

mat, woven roving and continuous strand, are selected for their physical properties, manufacturing characteristics and the chemical resistance of the laminate resulting from their use.

## Corrosion Barrier

The corrosion barrier of IntegraLine pipe is nominally 100 mils thick and is comprised of $70 \%$ to $80 \%$ resin. This highly resinated laminate is reinforced by one layer of "C" glass veil followed by two layers of randomly oriented fiber strand mat.

## Abrasion Barrier

## IntegraLine AR pipe starts with the

 same corrosion barrier described above, but includes $10-40 \%$ granular ceramic added to the resin. The granular ceramic material is the type used for manufacture of abrasive wheels and has a Knoop hardness of $2000-2500 \mathrm{Kg} / \mathrm{mm}^{2}$ (approximately 9 MOHS).
## Color

Pigmented exterior gel coats are not used on IntegraLine pipe unless specified by the customer. IntegraLine AR pipe will contain a pigment in the abrasionresistant liner(s) to contrast with the structural laminate in order that "wearthrough" from erosion is visible.

## Durability

The high tensile elongation properties of the vinyl ester resins utilized in IntegraLine pipe impart a superior toughness to the pipe enabling it to resist cracking and crazing of the resin when subjected to heavy design loads. In addition to high fatigue resistance, this toughness also provides a safety factor against impact damage during shipping and installation.

## Structural Laminate

## Straight Pipe

IntegraLine pipe is manufactured by the filament winding process utilizing continuous fiberglass strand wound in a helical pattern at a nominal 55 degree wind angle to produce an optimum combination of hoop and axial properties for most typical applications. The high glass content resulting from the filament winding process imparts excellent strength characteristics to the laminate providing superior protective structural backup to the resin rich corrosion barrier.

## Fittings

IntegraLine pipe fittings are manufactured utilizing a highly efficient contact-molded laminate consisting of alternating layers of glass fiber strand mat and bi-directional woven glass roving. The high glass content resulting from the specific laminating process used for IntegraLine pipe fittings permits the wall thickness of this hand-layup process to closely approximate the wall thickness of filament wound straight pipe in equivalent pressure rated classes.

## Filament Wound Laminate

Note: Corrosion/Abrasion Barrier may be thicker for specific applications.

11 c-Glass surface veil
(2) Chopped Strand Mat
(3) Woven Roving
(4) Filament Wound Strand
(5) Outer surface layer with U.V. inhibibior

50 PSI

| Diameter <br> (i..) | Total Wall <br> Thickness <br> (i..) | Unit <br> Weight <br> (b.) | Allowable <br> Vacuum <br> (ssi) | Max. Type I <br> Simple Span* <br> (f.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.21 | 2.74 | 5.80 | 14.7 |
| 8 | 0.21 | 3.69 | 2.50 | 13.9 |
| 10 | 0.21 | 4.57 | 1.28 | 13.0 |
| 12 | 0.21 | 5.46 | 0.73 | 12.0 |
| 14 | 0.21 | 6.35 | 0.46 | 10.7 |
| 16 | 0.26 | 9.23 | 0.92 | 14.8 |
| 18 | 0.26 | 10.36 | 0.64 | 13.9 |
| 20 | 0.26 | 11.49 | 0.47 | 12.9 |
| 24 | 0.31 | 16.73 | 0.60 | 15.7 |
| 30 | 0.31 | 20.83 | 0.31 | 12.8 |
| 36 | 0.36 | 29.38 | 0.33 | 15.0 |

## 100 PSI

| Diameter <br> (i.n.) | Total Wall <br> Thickness <br> (in.) | Unit <br> Weight <br> (b.) | Allowable <br> Vacuum <br> (psi) | Max. Type I <br> Simple Span* <br> (t.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.21 | 2.74 | 5.90 | 11.5 |
| 8 | 0.24 | 4.31 | 5.00 | 12.5 |
| 10 | 0.26 | 5.85 | 3.78 | 13.0 |
| 12 | 0.29 | 7.90 | 3.60 | 14.0 |
| 14 | 0.31 | 9.88 | 3.06 | 14.0 |
| 16 | 0.34 | 12.46 | 3.03 | 15.0 |
| 18 | 0.36 | 14.89 | 2.70 | 15.5 |
| 20 | 0.41 | 19.02 | 3.30 | 17.0 |
| 24 | 0.46 | 25.74 | 2.97 | 18.0 |
| 30 | 0.56 | 39.53 | 3.20 | 19.5 |
| 36 | 0.62 | 52.66 | 2.63 | 20.5 |

150 PSI

| Diameter <br> (i..) | Total Wall <br> Thickness <br> (in.) | Unit <br> Weight <br> (b.) | Allowable <br> Vacuum <br> (psi) | Max. Type I <br> Simple Span* <br> (t.) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.23 | 3.05 | 9.60 | 11.0 |
| 8 | 0.27 | 4.93 | 8.80 | 12.5 |
| 10 | 0.32 | 7.40 | 9.60 | 13.0 |
| 12 | 0.36 | 10.05 | 9.10 | 14.5 |
| 14 | 0.39 | 12.74 | 7.90 | 15.0 |
| 16 | 0.43 | 16.13 | 7.70 | 15.5 |
| 18 | 0.47 | 19.92 | 7.68 | 16.5 |
| 20 | 0.50 | 23.58 | 7.00 | 17.5 |
| 24 | 0.58 | 33.02 | 7.00 | 18.5 |
| 30 | 0.68 | 48.61 | 6.30 | 20.5 |
| 36 | 0.81 | 69.87 | 6.65 | 23.0 |

[^0]50 PSI

| Diameter | Pipe Total Wall Thickness | Pipe Unit Weight | Full Face Flange Thickness | 90 Ell | N I T Full Face Flange | $\begin{gathered} \text { W E I G H } \\ \substack{\text { Stub End } \\ \text { Flange }} \end{gathered}$ | T S Reducer (1 size red.) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 0.19 | 0.8 | 1/2 | 0.3 | 1.4 | 0.6 |  |
| 3 | 0.19 | 1.1 | 1/2 | 0.7 | 2.1 | 0.8 | 0.2 |
| 4 | 0.19 | 1.5 | 9/16 | 1.2 | 3.1 | 1.2 | 0.3 |
| 6 | 0.19 | 2.2 | 5/8 | 2.6 | 4.8 | 2.0 | 0.8 |
| 8 | 0.19 | 3.0 | 3/4 | 4.8 | 7.2 | 2.8 | 1.2 |
| 10 | 0.24 | 4.8 | 7/8 | 9.6 | 12.9 | 5.1 | 1.6 |
| 12 | 0.24 | 5.8 | 1 | 13.8 | 18.6 | 6.8 | 2.2 |
| 14 | 0.24 | 6.7 | 1-1/16 | 18.6 | 23.6 | 8.7 | 2.6 |
| 16 | 0.30 | 9.7 | 1-3/16 | 30.8 | 32.5 | 12.4 | 3.4 |
| 18 | 0.30 | 10.9 | 1-1/4 | 38.8 | 36.1 | 13.9 | 4.3 |
| 20 | 0.30 | 12.1 | 1-5/16 | 47.8 | 43.0 | 15.7 | 4.8 |
| 24 | 0.35 | 17.0 | 1-1/2 | 80.7 | 61.7 | 21.8 | 12.1 |
| 30 | 0.41 | 25.1 | 1-7/8 | 148.2 | 108.3 | 39.0 | 26.3 |
| 36 | 0.46 | 33.8 | 2-3/16 | 239.9 | 163.4 | 54.2 | 36.8 |

100 PSI

| Diameter | Pipe <br> Total Wall Thickness | Pipe Unit Weight | Full Face Flange Thickness |  | UN I T Full Face Flange | W E I G H <br> Stub End <br> Flange | T S <br> Reducer <br> (1 size red.) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 0.19 | 0.8 | 9/16 | 0.3 | 1.6 | 0.6 |  |
| 3 | 0.19 | 1.1 | 11/16 | 0.7 | 2.7 | 0.8 | 0.2 |
| 4 | 0.19 | 1.5 | 13/16 | 1.2 | 4.2 | 1.2 | 0.3 |
| 6 | 0.24 | 2.9 | 7/8 | 3.4 | 6.6 | 2.6 | 0.9 |
| 8 | 0.30 | 5.0 | 1 | 7.9 | 10.7 | 4.5 | 1.7 |
| 10 | 0.30 | 6.2 | 1-3/16 | 12.3 | 17.6 | 6.8 | 2.3 |
| 12 | 0.35 | 8.7 | 1-7/16 | 20.7 | 27.9 | 10.1 | 3.1 |
| 14 | 0.41 | 11.9 | 1-1/2 | 33.1 | 36.9 | 15.4 | 4.3 |
| 16 | 0.46 | 15.3 | 1-5/8 | 48.5 | 48.0 | 20.4 | 5.7 |
| 18 | 0.46 | 17.2 | 1-3/4 | 61.1 | 54.4 | 21.8 | 6.8 |
| 20 | 0.52 | 21.6 | 1-7/8 | 85.5 | 68.6 | 27.9 | 8.1 |
| 24 | 0.63 | 31.6 | 2-1/8 | 149.7 | 99.4 | 41.6 | 22.2 |
| 30 | 0.74 | 46.5 | 2-1/2 | 274.8 | 167.8 | 74.4 | 48.8 |
| 36 | 0.85 | 64.1 | 2-13/16 | 454.6 | 246.1 | 104.9 | 69.1 |

## 150 PSI

| Diameter | Pipe <br> Total Wall <br> Thickness |  | Full Face Flange Thickness | 90 Ell | N I T Full Face Flange | $\begin{aligned} & \text { W E I G H } \\ & \substack{\text { Stub End } \\ \text { Flange }} \end{aligned}$ | T S Reducer (1 size red.) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 0.19 | 0.8 | 11/16 | 0.3 | 1.8 | 0.6 |  |
| 3 | 0.24 | 1.5 | 13/16 | 0.9 | 3.3 | 1.1 | 0.2 |
| 4 | 0.24 | 2.0 | 15/16 | 1.5 | 5.0 | 1.5 | 0.4 |
| 6 | 0.30 | 3.7 | 1-1/16 | 4.4 | 8.2 | 3.4 | 1.2 |
| 8 | 0.35 | 5.9 | 1-1/4 | 9.4 | 13.3 | 5.3 | 2.1 |
| 10 | 0.46 | 9.8 | 1-7/16 | 19.4 | 23.7 | 10.7 | 3.3 |
| 12 | 0.52 | 13.3 | 1-3/4 | 31.6 | 37.1 | 15.3 | 4.8 |
| 14 | 0.57 | 16.9 | 1-7/8 | 47.0 | 49.4 | 21.7 | 6.3 |
| 16 | 0.63 | 21.4 | 2-1/16 | 67.7 | 64.7 | 28.3 | 8.0 |
| 18 | 0.68 | 26.0 | 2-1/4 | 92.4 | 76.6 | 32.8 | 9.9 |
| 20 | 0.74 | 31.4 | 2-7/16 | 124.1 | 96.1 | 40.3 | 12.0 |
| 24 | 0.85 | 43.3 | 2-13/16 | 205.1 | 139.2 | 56.7 | 31.1 |
| 30 | 1.07 | 68.3 | 3-3/8 | 404.0 | 245.4 | 108.9 | 69.7 |
| 36 | 1.23 | 94.2 | 4 | 668.1 | 376.8 | 153.6 | 101.6 |



NOTE: 1. Dimension $\mathrm{A}\left(90^{\circ}\right)$, or $\mathrm{B}\left(45^{\circ}\right)$ can be reduced with mitered construction.


Optional Flanged Elbows

3. Elbows can be provided with flange laminated to the pre-manufactured elbow, however these should be used only as a necessary alternative to the preferred configuration shown.

NOTES: 1. L = Standard Stub length unless specific length is requested.
2. Ellow with either full face flanges or flanges with steel backing rings.


Reducers


Notes: 1. Formula for length of reducer $L=2-1 / 2\left(D_{l} \cdot D_{S}\right)$
2. Formula for eccentric offset $E=\frac{D_{L}-D_{S}}{2}$
3. For length of standard flange see appropriate flange table.
4. Lengths other than those shown are available.


Reducers with full face flanges
The large end of the reducer can be provided
in flanged configuration.


Reducers are available with either full face
flanges or stub flanges with steel backing rings.

Pipe Design \& Selection

## Full Face and

 Blind Flanges

| $\begin{gathered} \text { ID } \\ \text { Diameter } \end{gathered}$ | OD* Outside Diameter | Number of Holes | Diameter of Holes | $\begin{aligned} & \text { BC } \\ & \text { Bolt } \\ & \text { circle } \end{aligned}$ | $\begin{aligned} & \text { Flange Thickness } \\ & 50 \mathrm{PSI} \stackrel{100}{ }{ }^{\text {PSI }} 150 \mathrm{PSI} \end{aligned}$ | Stub Length |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| 1-1/2 | 5 | 4 | 5/8 | 3-7/8 | 1/2 | 9/16 | 11/16 | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 6 | 4 | 3/4 | 4-3/4 | 1/2 | 9/16 | 11/16 | 6 |
| 2-1/2 | 7 | 4 | 3/4 | 5-1/2 | 1/2 | 11/16 | 3/4 | 6 |
| 3 | 7-1/2 | 4 | $3 / 4$ | 6 | 1/2 | 11/16 | 13/16 | 6 |
| 4 | 9 | 8 | 3/4 | 7-1/2 | 9/16 | 13/16 | 15/16 | 6 |
| 6 | 11 | 8 | 7/8 | 9-1/2 | 5/8 | 7/8 | 1-1/16 | 8 |
| 8 | 13-1/2 | 8 | 7/8 | 11-3/4 | 3/4 | 1 | 1-1/4 | 8 |
| 10 | 16 | 12 | 1 | 14-1/4 | 7/8 | 1-3/16 | 1-7/16 | 10 |
| 12 | 19 | 12 | 1 | 17 | 1 | 1-7/16 | 1-3/4 | 10 |
| 14 | 21 | 12 | 1-1/8 | 18-3/4 | 1-1/16 | 1-1/2 | 1-7/8 | 12 |
| 16 | 23-1/2 | 16 | 1-1/8 | 21-1/4 | 1-3/16 | 1-5/8 | 2-1/16 | 12 |
| 18 | 25 | 16 | 1-1/4 | 22-3/4 | 1-1/4 | 1-3/4 | 2-1/4 | 12 |
| 20 | 27-1/2 | 20 | 1-1/4 | 25 | 1-5/16 | 1-7/8 | 2-7/16 | 12 |
| 24 | 32 | 20 | 1-3/8 | 29-1/2 | 1-1/2 | 2-1/8 | 2-13/16 | 12 |
| 30 | 38-3/4 | 28 | 1-3/8 | 36 | 1-7/8 | 2-1/2 | 3-3/8 | 15 |
| 36 | 46 | 32 | 1-5/8 | 42-3/4 | 2-3/16 | 2-13/16 | 4 | 15 |
| $\begin{gathered} * T o l e r a n c e ~ o n ~ \\ 0 . D . \\ \text { is } \\ -0^{\prime \prime} \\ +1 / 2 " \end{gathered}$ |  |  |  |  |  |  |  |  |

Flange drilling per ANSI B16.1, Class 125 (identical to ANSI B16.5, Class 150 through 24 " dia.)


Stub Ends with
Steel Backing
Flanges

## Stub End

| ID |  | Flange Thickness |  |  | Stub Length |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Diameter | 50 PSI | 100 PSI | 150 PSI |  |


| 2 | 4 | $1 / 2$ | $1 / 2$ | $1 / 2$ | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | $5 \cdot 1 / 4$ | $1 / 2$ | $1 / 2$ | $9 / 16$ | 6 |
| 4 | $6 \cdot 3 / 4$ | $1 / 2$ | $9 / 16$ | $5 / 8$ | 6 |
| 6 | $8 \cdot 5 / 8$ | $1 / 2$ | $9 / 16$ | $3 / 4$ | 8 |
| 8 | $10 \cdot 7 / 8$ | $1 / 2$ | $11 / 16$ | $7 / 8$ | 8 |
| 10 | $13 \cdot 1 / 4$ | $9 / 16$ | $13 / 16$ | 1 | 10 |
| 12 | 16 | $9 / 16$ | $15 / 16$ | $1 \cdot 5 / 16$ | 10 |
| 14 | $17 \cdot 5 / 8$ | $5 / 8$ | $1 \cdot 1 / 16$ | $1 \cdot 3 / 8$ | 12 |
| 16 | $20 \cdot 1 / 8$ | $5 / 8$ | $1 \cdot 1 / 16$ | $1 \cdot 1 / 2$ | 12 |
| 18 | $21 \cdot 1 / 2$ | $3 / 4$ | $1 \cdot 1 / 8$ | $1 \cdot 5 / 8$ | 12 |
| 20 | $23 \cdot 3 / 4$ | $3 / 4$ | $1 \cdot 1 / 4$ | $1 \cdot 5 / 8$ | 12 |
| 24 | $28 \cdot 1 / 8$ | $7 / 8$ | $1 \cdot 1 / 2$ | $1 \cdot 3 / 4$ | 12 |
| 30 | $34 \cdot 5 / 8$ | $15 / 16$ | $1 \cdot 11 / 16$ | $2 \cdot 5 / 16$ | 15 |
| 36 | $41 \cdot 1 / 8$ | $1 \cdot 1 / 16$ | 2 | $2 \cdot 5 / 8$ | 15 |



## Steel Backing Flange

| Pipe Diameter | 50psi | $\begin{aligned} & \text { ID } \\ & \text { Inside Diameter } \\ & \text { 100psi } \end{aligned}$ | OD Outside Diameter | $B C$ Bolt Circle Diameter | Number of Holes | Diameter of Holes | Thickness | Approx. Weight* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 2-5/8 | ID's are for | 6 | 4-3/4 | 4 | 3/4 | 5/8 | 2.8 |
| 3 | 3-3/4 | SK-39-S0 | 7-1/2 | 6 | 4 | 3/4 | 5/8 | 4.5 |
| 4 | 4-3/4 | or | 9 | 7-1/2 | 8 | 3/4 | 5/8 | 6.5 |
| 6 | 7 | KK0.50 | 11 | 9-1/2 | 8 | 7/8 | 3/4 | 9.5 |
| 8 | 9 | Sk-O-SO | 13-1/2 | 11-3/4 | 8 | 7/8 | 3/4 | 12.5 |
| 10 | 11-1/8 |  | 16 | 14-1/4 | 12 | 1 | 7/8 | 19 |
| 12 | 13-1/8 | SK-70-9so | 19 | 17 | 12 | 1 | 7/8 | 28 |
| 14 | 15 |  | 21 | 18-3/4 | 12 | 1-1/8 | 1 | 32 |
| 16 | 17 |  | 23-1/2 | $21 \cdot 1 / 4$ | 16 | 1-1/8 | 1 | 42 |
| 18 | 19 | SPECIAL | 25 | 22-3/4 | 16 | 1-1/4 | $1 \cdot 1 / 8$ | 50 |
| 20 | 21 | BORE | 27-1/2 | 25 | 20 | 1-1/4 | 1-1/8 | 58 |
| 24 | 25 |  | 32 | 29-1/2 | 20 | 1-3/8 | 1-1/8 | 82 |
| 30 | 31-1/4 |  | 38-3/4 | 36 | 28 | 1-3/8 | 1-1/4 | 130 |
| 36 | 37-1/4 |  | 46 | 42-3/4 | 32 | 1-5/8 | 1-1/4 | 175 |

Flanged Joints

- Fastener

Requirements

full face flange connection

Steel Backing Flange


STUB FLANGE WITH STEEL backing flange connection


METAL RAISED FACE FLANGE TO FULL FACE FRP FLANGE CONNECTION


FULL FACE FLANGE TO STUB FLANGE WITH STEEL BACKING RING CONNECTION

NOTES: 1. Use full face or ring gasket as indicated in sketches. 2. Do not connect full face flanges to raised face or stub flanges withouta a spacer ring.

| Flange Diameter | Rated Pressure | Flange Thickness | Quantity Required | Diameter | Bolt Length |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 50 | 1/2 | 4 | 5/8 | 2-1/4 |
|  | 100 | 9/16 | 4 | 5/8 | 2-1/2 |
|  | 150 | 11/16 | 4 | 5/8 | 2-3/4 |
| 3 | 50 | 1/2 | 4 | 5/8 | 2-1/4 |
|  | 100 | 11/16 | 4 | 5/8 | 2-3/4 |
|  | 150 | 13/16 | 4 | 5/8 | 3 |
| 4 | 50 | 9/16 | 8 | 5/8 | 2-1/2 |
|  | 100 | 13/16 | 8 | 5/8 | 3 |
|  | 150 | 15/16 | 8 | 5/8 | 3-1/4 |
| 6 | 50 | 5/8 | 8 | 3/4 | 2-3/4 |
|  | 100 | 7/8 | 8 | 3/4 | 3-1/4 |
|  | 150 | 1-1/16 | 8 | 3/4 | 3-1/2 |
| 8 | 50 | 3/4 | 8 | 3/4 | 3 |
|  | 100 | 1 | 8 | 3/4 | 3-1/2 |
|  | 150 | 1-1/4 | 8 | 3/4 | 4 |
| 10 | 50 | 7/8 | 12 | 7/8 | 3-1/4 |
|  | 100 | 1-3/16 | 12 | 7/8 | 4 |
|  | 150 | 1-7/16 | 12 | 7/8 | 4-1/2 |
| 12 | 50 | 1 | 12 | 7/8 | 3-1/2 |
|  | 100 | 1.7/16 | 12 | 7/8 | 4-1/2 |
|  | 150 | 1-3/4 | 12 | 7/8 | 5 |
| 14 | 50 | 1-1/16 | 12 | 1 | 4 |
|  | 100 | 1-1/2 | 12 | , | 5 |
|  | 150 | 1-7/8 | 12 | 1 | 5-3/4 |
| 16 | 50 | 1-3/16 | 16 | 1 | 4-1/4 |
|  | 100 | 1-3/4 | 16 | 1 | 5-1/2 |
|  | 150 | 2-1/16 | 16 | 1 | 6 |
| 18 | 50 | 1-1/4 | 16 | 1-1/8 | 4-1/2 |
|  | 100 | 1-3/4 | 16 | 1-1/8 | 5-1/2 |
|  | 150 | 2-1/4 | 16 | 1-1/8 | 6-1/2 |
| 20 | 50 | 1-5/16 | 20 | 1-1/8 | 4-3/4 |
|  | 100 | 1-7/8 | 20 | 1-1/8 | 5-3/4 |
|  | 150 | 2-7/16 | 20 | 1-1/8 | 7 |
| 24 | 50 | 1-1/2 | 20 | 1-1/4 | 5-1/4 |
|  | 100 | 2-1/8 | 20 | 1-1/4 | 6-1/2 |
|  | 150 | 2-13/16 | 20 | 1-1/4 | 8 |
| 30 | 50 | 1-7/8 | 28 | 1-1/4 | 6 |
|  | 100 | 2-1/2 | 28 | 1-1/4 | 7-1/4 |
|  | 150 | 3-3/8 | 28 | 1-1/4 | 9 |
| 36 | 50 | 2.3/16 | 32 | 1-1/2 | 7 |
|  | 100 | 2-13/16 | 32 | 1-1/2 | 8-1/4 |
|  | 150 | 4 | 32 | 1-1/2 | 10-1/2 |

NOTES: 1. Bolt lengths are calculated for full face FRP flanges. Length requirements for stub ends with steel backing flanges may vary and should be verified with FIBREX.
2. Bolt lengths are adequate for (2) washers plus heavy hex nut and $1 / 8^{\prime \prime}$ thick gasket with excess of $3 / 8^{\prime \prime}-1 / 2^{\prime \prime}$.
3. Use ANSI Type A Narrow or Type B Narrow plain washers.
4. Use gaskets with Shore A durometer of $50-60$. Gaskets should be $1 / 8$ " minimum thickness up through 24 " diameter and $3 / 16$ " for 30 and 36 " diameter.


1. Gaskets should have a Shore A durometer of $50-60$ with the following minimum thickness; $1 / 8$ " thru 20" diameter, $3 / 16$ " 24" - 36" diameter.
2. Bolts should initially be fightened to $50 \%$ of the values shown. Subsequent tightening should be in the same sequence until the required torque is reached.

Typical Bolt Torque Force
Required for Sealing

| Pipe <br> Diameter <br> in. | 50 PSI | IO PSI <br> ft. - lb of torque |  |  | 150 PSI |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 25 | 25 | 25 |  |  |
| 3 | 25 | 25 | 25 |  |  |
| 4 | 25 | 25 | 25 |  |  |
| 6 | 25 | 25 | 40 |  |  |
| 8 | 25 | 40 | 60 |  |  |
| 10 | 25 | 40 | 70 |  |  |
| 12 | 25 | 45 | 80 |  |  |
| 14 | 30 | 60 | 100 |  |  |
| 16 | 30 | 70 | 120 |  |  |
| 18 | 35 | 80 | 130 |  |  |
| 20 | 35 | 90 | 140 |  |  |
| 24 | 40 | 100 | 150 |  |  |
| 30 | 45 | 120 | 175 |  |  |
| 36 | 50 | 140 | 200 |  |  |

NOTE: The indicated torque is suggested to seal flanges in pressure pipe using gaskets of a Shore A durometer of 50 to 60 .

Maximum Bolt Torque for Pressure Piping

| Bolt Size <br> in. | Torque <br> ft. - lb. |
| :---: | :---: |
| $1 / 2$ | 15 |
| $5 / 8$ | 25 |
| $3 / 4$ | 40 |
| $7 / 8$ | 65 |
| 1 | 100 |
| $1-1 / 8$ | 140 |
| $1-1 / 4$ | 200 |
| $1-1 / 2$ | 320 |
| $1-3 / 4$ | 600 |
| 2 | 880 |

Based on a 12,000 psi bolt stress. Use ANSI Type A Narrow or Type B Narrow plain washers.

Flanged Joints

- Bolting Torque and Sequence

Pipe Design \& Selection

## Fabricated

## Branch

Connections


| 2 | 6 | 6 | 10 | 16 |
| :---: | :---: | :---: | :---: | :---: |
| 3 | 7 | 6 | 12 | 18 |
| 4 | 8 | 6 | 14 | 20 |
| 6 | 10 | 8 | 16 | 24 |
| 8 | 12 | 10 | 20 | 30 |
| 10 | 14 | 10 | 24 | 34 |
| 12 | 16 | 12 | 26 | 38 |
| 14 | 18 | 12 | 30 | 42 |
| 16 | 20 | 14 | 32 | 46 |
| 18 | 21 | 14 | 36 | 50 |
| 20 | 22 | 16 | 38 | 54 |
| 24 | 24 | 18 | 42 | 60 |
| 30 | 30 | 20 | 52 | 72 |
| 36 | 33 | 22 | 62 | 84 |

NOTES: 1. A is the minimum recommended length to allow for a joint overlay.
2. Tees, including reducing tees, are not one-piece construction but are manufactured by joining one section of pipe into the sidewall of another. For this reason it is rarely of benefit to order a tee fitting as an individual component. The main run of pipe can be provided with the required branch line stub thereby saving shop and field joints.

Pipe Coupling Connection

| NPT | $A$ |
| :---: | :---: |
|  |  |
| $1 / 4$ | $3^{\prime \prime}$ |
| $3 / 8$ | $3^{\prime \prime}$ |
| $1 / 2$ | $3-1 / 2^{\prime \prime}$ |
| $3 / 4$ | $3-1 / 2^{\prime \prime}$ |
| 1 | $4^{\prime \prime}$ |
| $1-1 / 4$ | $4^{\prime \prime}$ |
| $1-1 / 2$ | $4-1 / 2^{\prime \prime}$ |




Friction Losses of Fittings in Equivalent Length of Straight Pipe

| Fitting - Diameter | 2 | 3 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 24 | 30 | 36 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 90 Smooth Turn Ell | 3 | 4 | 5 | 8 | 11 | 13 | 16 | 17 | 20 | 23 | 25 | 30 | 37 | 45 |
| 45 Smooth Turn Ell | 2 | 2 | 3 | 4 | 6 | 7 | 9 | 10 | 11 | 12 | 14 | 17 | 21 | 25 |
| Tee - Through Flow | 4 | 5 | 7 | 10 | 14 | 17 | 20 | 22 | 25 | 28 | 32 | 38 | 47 | 57 |
| Tee - Branch Flow | 11 | 16 | 20 | 30 | 40 | 50 | 60 | 66 | 75 | 85 | 95 | 113 | 140 | 170 |

IntegraLine pipe has excellent corrosion resistance and mechanical properties. However, as with any piping material, good application design and installation practices will greatly enhance the reliability and service life of the pipe system.

The following suggestions describe a rudimentary approach to laying out the piping system. This approach does not include all possible contingencies and is not intended to replace more extensive design approaches, such as finite element analysis, when the designer judges these to be appropriate.

## Supports

1. Select preliminary support locations. Steel supports for IntegraLine pipe should be spaced at maximum intervals shown in the tables on page 17. These distances should not be exceeded. A reduction of $10 \%$ in the distance between supports should be considered when:
(a) pipe is carrying fluids with specific gravities in the range of 1.1 to 1.3
(b) fluid contents of the pipe may be over 180 degrees Fahrenheit
(c) wind loads, vibration or other factors present may increase loads on the pipe run
2. Use support saddles of adequate size to eliminate the possibility of point loading. A good rule of thumb is that saddles should provide complete 180 degree support of the lower half of the pipe. Saddle length should be equal to the diameter of the pipe for small sizes and not less than two thirds the diameter of the pipe for larger sizes.
3. Valves, pumps, and other heavy equipment connected to the pipe should be supported independently to avoid imposing excessive loads on the pipe.
4. Vertical pipe runs should be supported from below so that pipe is "in compression".
5. A minimum $1 / 8$ " thick layer of neoprene or other elastomeric material should be provided between the pipe and the steel support saddle to insure maximum contact and to prevent abrasion. Thicker layers may be used to fill any excess space between the outside wall of the pipe and the interior curvature of the saddle.
6. When long runs of pipe are hung from overhead structures, guides should be incorporated periodically (every third or fourth hanger location) to provide lateral stability.

## Expansion \& Contraction

IntegraLine pipe expands in the axial direction at approximately twice the rate of steel. However, because it has a relatively low axial modulus of elasticity, thermal forces are smaller and therefore restraining anchors and guides need not be as heavy as for steel pipe.

Common practice for above-ground piping systems is to provide anchors at approximately 300 ft . intervals. This helps to prevent pipe movement due to vibration or water hammer. In addition to the natural anchor points in the system, such as equipment connections, it is a good idea to provide anchors
at transition points where changes in pipe diameter, direction or elevation, material of construction or major branch connections occur. This serves to divide the piping system into individual expanding sections that are simpler to deal with.

Expansion and contraction are usually handled by one or a combination of the following methods:

## 1. Directional Changes in the System.

 When sufficient flexibility exists within the piping system layout, using directional changes is generally the least expensive means to accommodate expansion and contraction. A typical approach to this method is described on page 18.2. Mechanical Expansion Joints. Various types of expansion joints are used successfully with FRP pipe. The following points should be considered when selecting an expansion joint:
(a) Because thermal forces developed are much lower than for steel pipe, it is essential to use an expansion joint which is activated by low forces. The force required to compress the expansion joint must not be greater than the force shown in the Compressive End Loads table on page 21.
(b) In installations where the pipe may operate at a lower temperature than the installation temperature, it may be necessary to pre-set the expansion joint for contraction.
(c) Guides should be installed to assure that the pipe will remain aligned through the expansion joint. Locate guides not more than 4 times the diameter of the pipe on either side of the expansion joint.
3. Expansion loops. This approach consists of an arc of pipe that flexes to accommodate changes in length. The design method is based on stress developed in a cantilevered beam with a concentrated load at the free end. It ignores flexibility of the loop leg parallel to the pipe line. Guidance for sizing of expansion loops is given on page 20.
4. Anchor supports and guides. For very short pipe runs and/or small changes in temperature, it is frequently unnecessary to make provisions for thermal expansion. The system designer should be aware however, that when pipe is restrained by anchor supports in lieu of providing other means to accommodate expansion, both pipe and anchor supports will be subjected to the end loads shown in the Compressive End Loads table on page 21. Supporting structural steel and steel anchor supports must therefore be capable of resisting these forces. When longer runs of pipe are restrained in this manner, it is necessary to provide guides to keep the pipe line straight, thereby directing forces in an axial direction to prevent buckling which might otherwise occur. Maximum guide spacing is given in the table on page 20. FRP thrust collars are laminated to the pipe on either side of an anchor support to restrain the pipe and are also used with riser
clamps for vertical support. Collars are generally applied while the pipe is being manufactured but can also be applied in the field.

## Water Hammer

The high pressure surge or shock load known as "water hammer" is produced by abrupt changes in fluid velocity within the pipe. The usual causes are instantaneous valve closing or opening, as well as pump start-up or shutdown. Pressure gauges, due to slow response time, frequently do not register water hammer pressure surges however violent vibration or movement in the pipeline can sometimes be observed. Complete explanations and calculations for this phenomenon can be found in piping handbooks. Under certain conditions these shock forces can be of sufficient magnitude to rupture a piping system. The system designer is cautioned to take measures to prevent or reduce these forces. One method would be to use slow-closing valves or surge tanks. Additionally, pumps should never be started into empty discharge lines unless valves are used to control flow. A check valve should be installed to control the velocity of liquid flowing back through a line. As a general guideline, IntegraLine pipe will withstand a dynamic pressure increase equal to the pressure rating of the pipe, however the system must be adequately anchored and supported, particularly at changes in direction and branch connections, to prevent movement of the pipeline.

## Vibration

Although low-amplitude vibration from a well-anchored centrifugal pump will generally have little effect on IntegraLine pipe, adjacent supports should be well cushioned to prevent abrasion of the exterior of the pipe. Large amplitude vibration should be isolated from the pipe through the use of flexible connectors.

## Hydrostatic Testing

Whenever possible, FRP piping systems should be hydrostatically tested prior to process start-up. Testing with air or gas is extremely hazardous and is not recommended. The following approach to testing the system is suggested:

1. Insure that all supports, guides and anchors are in place and the line is properly restrained.
2. Introduce water to the system at the lowest point, preferably through a 1" diameter or smaller pipe.
3. Provide a means to bleed air off, such as loosening a flange or partially opening a valve, at the highest point in the system.
4. When the system is filled, slowly close the air bleed-off point and gradually bring the system up to the desired pressure.
5. Test pressure should not exceed 1-1/2 times the system operating pressure or $1-1 / 2$ times the rated operating pressure of the pipe.

## System <br> Design

Allowable Spans
Between Supports

50 PSI

| Diameter | Wall <br> Thickness | Type I | Type II | Type III | Type IV |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.21 | 14.7 | 16.4 | 15.8 | 18.0 |
| 8 | 0.21 | 13.9 | 15.6 | 15.0 | 17.0 |
| 10 | 0.21 | 13.0 | 14.6 | 14.1 | 16.0 |
| 12 | 0.21 | 12.0 | 13.4 | 12.9 | 14.7 |
| 14 | 0.21 | 10.7 | 11.9 | 11.5 | 13.0 |
| 16 | 0.26 | 14.8 | 16.5 | 16.0 | 18.1 |
| 18 | 0.26 | 13.9 | 15.5 | 15.0 | 17.0 |
| 20 | 0.26 | 12.9 | 14.4 | 13.9 | 15.8 |
| 24 | 0.31 | 15.7 | 17.5 | 17.0 | 19.2 |
| 30 | 0.31 | 12.8 | 14.2 | 13.8 | 15.7 |
| 36 | 0.36 | 15.0 | 16.8 | 16.2 | 18.3 |

100 PSI

| Diameter | Wall <br> Thickness | Type I | Type II | Type III | Type IV |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.21 | 11.5 | 12.9 | 12.4 | 14.1 |
| 8 | 0.24 | 12.5 | 14.0 | 13.5 | 15.3 |
| 10 | 0.26 | 13.0 | 14.5 | 14.0 | 15.9 |
| 12 | 0.29 | 14.0 | 15.6 | 15.1 | 17.1 |
| 14 | 0.31 | 14.0 | 15.6 | 15.1 | 17.1 |
| 16 | 0.34 | 15.0 | 16.7 | 16.2 | 18.3 |
| 18 | 0.36 | 15.5 | 17.3 | 16.5 | 18.9 |
| 20 | 0.41 | 17.0 | 19.0 | 18.3 | 20.7 |
| 24 | 0.46 | 18.0 | 20.1 | 19.4 | 22.0 |
| 30 | 0.56 | 19.5 | 21.7 | 21.0 | 23.8 |
| 36 | 0.62 | 20.5 | 22.9 | 22.1 | 25.1 |

## 150 PSI

| Diameter | Wall <br> Thickness | Type I | Type II | Type III | Type IV |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.26 | 11.0 | 12.3 | 11.8 | 13.2 |
| 8 | 0.31 | 12.5 | 13.8 | 13.5 | 15.2 |
| 10 | 0.31 | 13.0 | 14.5 | 14.0 | 15.9 |
| 12 | 0.36 | 14.5 | 16.2 | 15.6 | 17.6 |
| 14 | 0.41 | 15.0 | 16.6 | 16.2 | 18.3 |
| 16 | 0.45 | 15.5 | 17.3 | 16.6 | 18.9 |
| 18 | 0.47 | 16.5 | 18.4 | 17.8 | 20.2 |
| 20 | 0.52 | 17.5 | 19.5 | 18.9 | 21.3 |
| 24 | 0.58 | 18.5 | 20.5 | 19.9 | 22.5 |
| 30 | 0.71 | 20.5 | 22.5 | 22.1 | 25.0 |
| 36 | 0.81 | 23.0 | 25.0 | 24.6 | 28.0 |

Type I
Simply supported spans (two supports per span length) with the run attached to a fiting of one end, or any other section of less than three span lengths.

(17)

## System <br> Direction <br> Changes



## Using System Direction Changes (Offset Legs) to Deal with Expansion

The illustration above depicts a typical installation configuration. To use this particular configuration to advantage in allowing for pipe expansion, the following steps would be appropriate:

1. Using the Linear Thermal Expansion table (Page 19), determine the maximum expansion of line 1 from any prior anchor point. This value is used with the Minimum Length of Offset Leg table (page 19) to find the minimum length of the offset leg B.
2. Determine the maximum expansion of that portion of line 2 between the anchor support and the lower elbow. This value is then used to find the minimum length of the offset leg A .
3. Determine the maximum expansion of line 3 from any prior anchor point and use this value to find the minimum length of the offset leg C. (Note: If the upper support location on the vertical run did not allow for an adequate distance to the upper elbow, it can be allowed to slide and the distance from the upper elbow to the anchor support then becomes the offset leg.)
4. Determine the maximum expansion from the anchor support to the upper elbow and use this value to find the minimum length of the offset leg $D$.

NOTES: 1. Generally, the support which satisfies the minimum offset leg length should prevent lateral movement and buckling. A Guide Support is frequently used for this purpose.
2. After determining the minimum allowable distance of the offset leg, check the Allowable Span table (page 16) to determine if additional supports between the elbow and the offset leg guide support are required. These should be sliding supports, allowing for both axial and lateral movement.
3. Steel supports, which satisfy the more commonly encountered requirements, are available from FIBREX and are shown in this manual.

Linear Thermal Expansion
Change in Temperature - Degrees F

| 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 | 140 | 150 | 160 | 170 | 180 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.1 | 0.3 | 0.4 | 0.5 | 0.7 | 0.8 | 1.0 | 1.1 | 1.2 | 1.4 | 1.5 | 1.6 | 1.8 | 1.9 | 2.1 | 2.2 | 2.3 | 2.5 |

Minimum Length of Offset Leg
Deflection of Offset Leg - (Linear expansion of main run) - inches

|  | 0.5 | 1.0 | 1.5 | 2 | 2.5 | 3 | 3.5 | 4 | 4.5 | 6 | 6.5 | 7 | 7.5 | 8 | 8.5 | 9 | 9.5 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 7.6 | 11 | 13 | 15 | 17 | 19 | 20 | 22 | 23 | 26 | 28 | 29 | 30 | 31 | 32 | 32 | 33 | 34 |
| 8 | 8.8 | 12 | 15 | 18 | 20 | 22 | 23 | 25 | 26 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 |
| 10 | 9.8 | 14 | 17 | 20 | 22 | 24 | 26 | 28 | 29 | 34 | 35 | 37 | 38 | 39 | 40 | 42 | 43 | 44 |
| 12 | 11 | 15 | 19 | 21 | 24 | 26 | 28 | 30 | 32 | 37 | 39 | 40 | 41 | 43 | 44 | 45 | 47 | 48 |
| 14 | 12 | 16 | 20 | 23 | 26 | 28 | 30 | 33 | 35 | 40 | 42 | 43 | 45 | 46 | 47 | 49 | 50 | 51 |
| 16 | 12 | 17 | 21 | 25 | 28 | 30 | 33 | 35 | 37 | 43 | 44 | 46 | 48 | 49 | 51 | 52 | 54 | 55 |
| 18 | 13 | 18 | 23 | 26 | 29 | 32 | 34 | 37 | 39 | 45 | 47 | 49 | 50 | 52 | 54 | 55 | 57 | 58 |
| 20 | 14 | 19 | 24 | 27 | 31 | 34 | 36 | 39 | 41 | 48 | 49 | 51 | 53 | 55 | 57 | 58 | 60 | 61 |
| 24 | 15 | 21 | 26 | 30 | 34 | 37 | 40 | 42 | 45 | 52 | 54 | 56 | 58 | 60 | 62 | 64 | 65 | 67 |
| 30 | 17 | 24 | 29 | 33 | 37 | 41 | 44 | 47 | 50 | 58 | 60 | 63 | 65 | 67 | 69 | 71 | 73 | 75 |
| 36 | 18 | 26 | 32 | 37 | 41 | 45 | 48 | 52 | 55 | 63 | 66 | 69 | 71 | 73 | 76 | 78 | 80 | 82 |



## System <br> Design



Where straight runs with anchors at both ends are required, system direction changes (offset legs) can be replaced by an expansion loop to accommodate changes in length due to expansion. This is similar to creating "back-to-back offset legs".
The following steps are used to determine appropriate dimensions for an expansion loop:

1. Determine an available location for the expansion loop. It is not mandatory that the loop is equidistant between the two anchors however to the extent this is possible, the size of the loop will be minimized.
2. Determine the maximum change in temperature between the installation temperature and highest (or lowest) operating temperature.
3. Determine the distance between the expansion loop location and the farther of the two anchor supports.
4. Refer to the Minimum Length Of Offset Leg table (page 19) to determine the minimum length of leg " A ".
5. Leg length " $B$ " should not be less than one half the length of "A".
6. The distance to the first guide on either side of the loop should be no more than 4 times the diameter of the pipe and distance to the second guide, no more than 16 times the pipe diameter.
7. A support under leg " B " may be provided, however, do not provide any guides within the loop which could constrain pipe movement in the direction of the pipe run.

Maximum Guide Spacing in Feet

|  |  |  |  |  |  |  | Chang | Tem | ature | egrees |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 | 140 | 150 | 160 | 170 | 180 |
| Diameter |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 55 | 39 | 32 | 27 | 24 | 22 | 21 | 19 | 18 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 13 | 13 |
| 8 | 73 | 52 | 42 | 37 | 33 | 30 | 28 | 26 | 24 | 23 | 22 | 21 | 20 | 20 | 19 | 18 | 18 | 17 |
| 10 | 90 | 64 | 52 | 45 | 40 | 37 | 34 | 32 | 30 | 29 | 27 | 26 | 25 | 24 | 23 | 23 | 22 | 21 |
| 12 | 108 | 76 | 62 | 54 | 48 | 44 | 41 | 38 | 36 | 34 | 32 | 31 | 30 | 29 | 28 | 27 | 26 | 25 |
| 14 | 125 | 88 | 72 | 63 | 56 | 51 | 47 | 44 | 42 | 40 | 38 | 36 | 35 | 33 | 32 | 31 | 30 | 29 |
| 16 | 143 | 101 | 82 | 71 | 64 | 58 | 54 | 51 | 48 | 45 | 43 | 41 | 40 | 38 | 37 | 36 | 35 | 34 |
| 18 | 160 | 113 | 92 | 80 | 72 | 65 | 61 | 57 | 53 | 51 | 48 | 46 | 44 | 43 | 41 | 40 | 39 | 38 |
| 20 | 178 | 126 | 102 | 89 | 79 | 72 | 67 | 63 | 59 | 56 | 54 | 51 | 49 | 47 | 46 | 44 | 43 | 42 |
| 24 | 213 | 150 | 123 | 106 | 95 | 87 | 80 | 75 | 71 | 67 | 64 | 61 | 59 | 57 | 55 | 53 | 52 | 50 |
| 30 | 265 | 187 | 153 | 132 | 118 | 108 | 100 | 94 | 88 | 84 | 80 | 76 | 73 | 71 | 68 | 66 | 64 | 62 |
| 36 | 317 | 224 | 183 | 159 | 142 | 129 | 120 | 112 | 106 | 100 | 96 | 92 | 88 | 85 | 82 | 79 | 77 | 75 |



## System Design

## 50 PSI

## Compressive End <br> Loads due to <br> Thermal Expansion

|  | $25^{\circ}$ | $50^{\circ}$ | $75^{\circ}$ | $100^{\circ}$ | $125^{\circ}$ | $150^{\circ}$ | $175^{\circ}$ | $200^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter |  |  |  |  |  |  |  |  |
| 6 | 793 | 1586 | 2379 | 3172 | 3965 | 4758 | 5551 | 6344 |
| 8 | 1060 | 2120 | 3180 | 4240 | 5300 | 6360 | 7420 | 8480 |
| 10 | 1311 | 2623 | 3934 | 5246 | 6557 | 7868 | 9180 | 10491 |
| 12 | 1563 | 3125 | 4688 | 6251 | 7814 | 9376 | 10939 | 12502 |
| 14 | 1814 | 3628 | 5442 | 7256 | 9070 | 10884 | 12699 | 14513 |
| 16 | 3013 | 6027 | 9040 | 12054 | 15067 | 18080 | 21094 | 24107 |
| 18 | 3379 | 6758 | 10137 | 13516 | 16895 | 20274 | 23653 | 27032 |
| 20 | 3745 | 7489 | 11234 | 14978 | 18723 | 22467 | 26212 | 29957 |
| 24 | 5886 | 11773 | 17659 | 23546 | 29432 | 35319 | 41205 | 47091 |
| 30 | 7326 | 14652 | 21978 | 29304 | 36630 | 43956 | 51282 | 58608 |
| 36 | 10867 | 21735 | 32602 | 43469 | 54337 | 65204 | 76071 | 86939 |
| Restraining pipe expansion with anchors in these temperature ranges will result in excessive axial pipe stresses |  |  |  |  |  |  |  |  |

## 100 PSI

|  | $25^{\circ}$ | $50^{\circ}$ | $75^{\circ}$ | $100^{\circ}$ | $125^{\circ}$ | $150^{\circ}$ | $175^{\circ}$ | $200^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter |  |  |  |  |  |  |  |  |
| 6 | 793 | 1586 | 2379 | 3172 | 3965 | 4758 | 5551 | 6344 |
| 8 | 1354 | 2708 | 4062 | 5416 | 6770 | 8124 | 9478 | 10832 |
| 10 | 1917 | 3833 | 5750 | 7666 | 9583 | 11500 | 13416 | 15333 |
| 12 | 2717 | 5433 | 8150 | 10867 | 13583 | 16300 | 19016 | 21733 |
| 14 | 3487 | 6974 | 10462 | 13949 | 17436 | 20923 | 24411 | 27898 |
| 16 | 4542 | 9084 | 13626 | 18168 | 22710 | 27252 | 31794 | 36336 |
| 18 | 5521 | 11041 | 16562 | 22082 | 27603 | 33123 | 38644 | 44164 |
| 20 | 7308 | 14616 | 21925 | 29233 | 36541 | 43849 | 51158 | 58466 |
| 24 | 10153 | 20305 | 30458 | 40611 | 50764 | 60916 | 71069 | 81222 |
| 30 | 16179 | 32357 | 48536 | 64715 | 80893 | 97072 | 113251 | 129430 |
| 36 | 21889 | 43778 | 65667 | 87556 | 109446 | 131335 | 153224 | 175113 |
| Restraining pipe expansion with anchors in these temperature ranges will result in excessive axial pipe stresses |  |  |  |  |  |  |  |  |

150 PSI

| Temperature Change - degrees F |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $25^{\circ}$ | $50^{\circ}$ | $75^{\circ}$ | $100^{\circ}$ | $125^{\circ}$ | $150^{\circ}$ | $175^{\circ}$ | $200^{\circ}$ |
| Diameter |  |  |  |  |  |  |  |  |
| 6 | 940 | 1880 | 2820 | 3761 | 4701 | 5641 | 6581 | 7521 |
| 8 | 1650 | 3300 | 4950 | 6600 | 8250 | 9899 | 11549 | 13199 |
| 10 | 2650 | 5301 | 7951 | 10602 | 13252 | 15903 | 18553 | 21203 |
| 12 | 3738 | 7477 | 11215 | 14953 | 18691 | 22430 | 26168 | 29906 |
| 14 | 4842 | 9684 | 14527 | 19369 | 24211 | 29053 | 33895 | 38738 |
| 16 | 6279 | 12558 | 18838 | 25117 | 31396 | 37675 | 43954 | 50234 |
| 18 | 7903 | 15805 | 23708 | 31611 | 39513 | 47416 | 55319 | 63221 |
| 20 | 9471 | 18942 | 28413 | 37884 | 47356 | 56827 | 66298 | 75769 |
| 24 | 13603 | 27206 | 40808 | 54411 | 68014 | 81617 | 95219 | 108822 |
| 30 | 20479 | 40957 | 61436 | 81915 | 102394 | 122872 | 143351 | 163830 |
| 36 | 30041 | 60082 | 90124 | 120165 | 150206 | 180247 | 210288 | 240330 |

## System <br> Design

## Saddle Supports



Saddle Support

| Pipe Size | L |
| :---: | :---: |
| $6-10$ | 10 |
| $12-16$ | 12 |
| $18-20$ | 14 |
| 24 | 20 |
| 30 | 20 |
| 36 | 24 |

Order Guide Bands separately when required.


Anchor Support


| $6 \cdot 10$ | 10 | $1 / 2$ | 6 |
| :---: | :---: | :---: | :---: |
| $12 \cdot 16$ | 12 | $5 / 8$ | 8 |
| $18-20$ | 14 | $5 / 8$ | 8 |
| 24 | 16 | $3 / 4$ | 10 |
| 30 | 20 | $7 / 8$ | 12 |
| 36 | 24 | 1 | 14 |


| Clevis Hanger |  |
| :---: | :---: |
| Pipe Size | L |
|  |  |
| $6-14$ | 12 |
| $16-20$ | 14 |
| 24 | 16 |
| 30 | 20 |
| 36 | 24 |



Clamp Hanger

| Pipe Size | L |
| :---: | :---: |
| $6-14$ | 12 |
| $16-20$ | 14 |
| 24 | 16 |
| 30 | 20 |
| 36 | 24 |



Riser Clamp

| Pipe Size | E | T | W |
| :---: | :---: | :---: | :---: |
| $6 \cdot 10$ | 3 | $1 / 2$ | 3 |
| $12 \cdot 16$ | 4 | $5 / 8$ | 4 |
| $18-20$ | 4 | $5 / 8$ | 4 |
| 24 | 6 | $3 / 4$ | 6 |
| 30 | 8 | $7 / 8$ | 6 |
| 36 | 8 | 1 | 8 |



Integraline steel supports are avilable from Fibrex or can be provided by customer.


## Joining Procedures

IntegraLine pipe makes use of the joint type widely recognized as being the most corrosion resistant and reliable of all currently available means of connecting FRP pipe components... the BUTT JOINT, sometimes also known as the "butt wrap" joint or the "butt and strap" joint. This type of joint is analogous to a weld in metallic piping systems and consists essentially of a "strap" of laminate wrapped around the exterior of the two parts being joined. This joint uses the same materials of construction as the pipe fittings. The result is a homogeneous "weld", without the potential for problems sometimes associated with systems utilizing various adhesives, mechanical components or other materials of dissimilar composition. Since IntegraLine pipe is not about compromises, FIBREX strongly recommends the use of the BUTT JOINT rather than seemingly more convenient, but potentially less reliable, alternative types of joints.
It may take days to become proficient at welding stainless steel, but it takes only a few hours to become an expert at "welding" FRP pipe.

## Before You Start...

you will need:

1. for weighing and measuring

- graduated cylinder ( metric )
- weighing scale (25lb to 60 lb capacity)
- floor paper, flexible plastic strip or other material to wrap around pipe

2. for cutting and surface preparation

- power sander and sanding discs (24 grit \& 60 grit )
- barrel grinder
- circular saw (diamond coated or carbide grit masonry blade)
- saber saw or hack saw (carbide tip or grit blade) if irregular cuts will be required

3. for applying laminate materials

- stiff bristle brushes
- $3^{\text {" }}$ wide laminating roller (bristle or metal fin)
- 6 " wide paint rollers
- scissors
- razor trim knife
- mixing sticks
- putty knife
- several gallon and pint containers
- clean rags
- pails for storage of rollers and brushes in
- cleaning agent
- acetone or water based emulsifier for cleaning tools
- cardboard sheets or floor paper to wet out glass strips

The following step-by-step procedures will produce a no-compromise, "welded" BUTT JOINT assuring the integrity of the system.

1. Wrap the flexible plastic strip, heavy floor paper or other sheet material around pipe to act as a template for marking a true square cut.
2. With pipe properly supported, cut ends square using the circular saw. If irregular cuts are required, use a saber saw or hack saw.
3. Sand the exterior surface of the pipe using a power sander with 24 grit disc to remove all of the resin wax coat for a distance at least $1^{\prime \prime}$ beyond the completed strap overlay width.
4. Maximum chemical resistance of the joint is achieved with an INSIDE OVERLAY. This can be provided on all joints where the pipe is large enough to allow entry or the joint can be reached from outside the pipe. If an INSIDE OVERLAY is to be provided, lightly sand the inside of the pipe back a distance 1 " beyond the completed inside overlay width. Sanding should not disturb the C -veil in the inner surface of the pipe but merely roughen the smooth mold surface of the resin to allow the INSIDE OVERLAY to bond with it.
5. The cut edges of the pipe should be prepared in the following manner.
NOTE: If an INSIDE OVERLAY cannot be provided, protection of the cut edges is particularly important and the following procedure should be performed with due care and attention to detail. If the pipe was cut more than 4 hours previously or has been contaminated with dust or other debris, lightly sand the square edge of the pipe to reveal previously unexposed laminate. Using a stiff bristle brush, coat the cut edges with the appropriate resin formulation so that no glass fibers are exposed and all voids are filled. Two or more coats may be advisable.
6. Align the two sections of pipe to be joined. It is imperative that they are supported firmly enough to prevent any movement after starting lamination (fig. 6).
7. When field joint kits are purchased from FIBREX, the resin will already be promoted and ready to mix in accordance with the following guidelines. Resin for "puttying" will have a thickener in it and resin for the exterior will already have the wax mixed in. These materials are also available from your local DERAKANE distributor, however resin purchased directly from a distributor may not be promoted. Ask the distributor to promote the resin and add thickener, wax and U.V. stabilizer, as required, or promote on site in accordance with resin manufacturer's instructions (available from the distributor or from FIBREX). NOTE: "Pot life" is the time between catalyzation and set-up. Adjust the quantity of catalyst to compensate for ambient temperature conditions or to provide a desired pot life. The table below is based on an ambient temperature of 70 degrees F. For every 15 degrees above 70 degrees $F$., the pot life will be cut approximately in half. For every 15 degrees below 70 degrees F., the pot life will be approximately double. If pot life exceeds 1 hour, external heat may be required to produce a complete cure. Using too little catalyst can result in an incomplete cure. Less than 1 part per hundred ( $1 \%$ or $4.5 \mathrm{cc} / \mathrm{lb}$ ) is not recommended.
8. Start by mixing an adequate amount of the putty resin to fill any gaps or irregularities and apply it to the joint, forcing it into the crevice between the two pieces of pipe.
It is not necessary to force putty all the way to the inside of the pipe as this could result in obstructions to the flow. Scrape any excess off the exterior of the pipe, leaving a smooth surface. If small diameter pipe is being joined, this should be adequate to hold the sections of pipe together.
9. If large diameter pipe is being joined, it is helpful to add HOT PATCHES to assist in holding the pipes together. Cut 3 or more pieces of mat, 2"-3" square, saturate with the hot patch resin and place across the joint in 3 or more places to "tack weld" the pipes together.
10. Before proceeding, jab the putty and HOT PATCHES lightly with a knife point to determine if they are cured. Cured material will be hard. If it is soft or spongy, it needs more time. If it does not get hard it was not properly mixed and the prior steps will need to be done over.

## 11. If you are applying an INSIDE

 OVERLAY, take the plies of glass for the corrosion barrier (one C-veil and two mat) and set them aside until after completion of the EXTERIOR OVERLAY. If an INSIDE OVERLAY is not possible, include the corrosion barrier plies with the other plies to be applied to the exterior of the pipe in step no. 12. Prior to commencing the EXTERIOR OVERLAY, check to insure that all prepared surfaces are clean and free of moisture, dirt, oils and waxes. If necessary, hand sand or power sand to remove any contaminants.

## Resin Formulation Chart

|  | Hot patch \& putty resin | Laminating resin | Exterior wax coat resin |
| :--- | :---: | :---: | :---: |
| Resin | 100 parts | 100 parts | 100 parts |
| Catalyst (MEKP) | 3 parts | $11 / 4$ parts | 2 parts |
|  | $(10-12 \mathrm{cc} / \mathrm{lb})$ | $(5-6 \mathrm{cc} / \mathrm{b})$ | $(8-9 \mathrm{cc} / \mathrm{lb})$ |
| Pot Life | 12 min. | $20-40 \mathrm{~min}$. | $15-25 \mathrm{~min}$. |


12. Mix the laminating resin and apply with brush or paint roller to all prepared (sanded) areas of the joint (12a). Commence wetting out the glass "strap", working on clean cardboard or floor paper. Start with the narrowest ply (strip) of glass and apply resin to it, rolling until uniformly saturated (12b). Place the glass ply around the joint, being careful to have it centered. (12c), and roll all the air out using a laminating roller, rolling from the center toward the edges of the glass (12d). Add more resin, if necessary, using a brush or paint roller. Repeat this procedure with each consecutively wider glass ply (strip) until the joint is completed. Subsequent layers of glass should lap at different locations around the pipe. Care must be taken to prevent the joint laminate from sagging at the bottom of the pipe during the curing process.

After acquiring an adequate level of experience, you will want to substitute the following procedure, or one like it, for wetting and applying the glass to the joints. This will appreciably speed up the process. Determine how many layers of glass you can apply together at one time. Place the widest on the cardboard or floor paper, apply resin and roll on it to completely saturate it and remove air bubbles. Center the next, slightly narrower glass ply on top of it but offsetting $1 / 2^{\prime \prime}-1^{\prime \prime}$ on the length. Apply resin and roll on it. Repeat this procedure with each successive glass ply until the narrowest has been rolled out (12e). Note: when using this procedure, it is more important to roll air out of the laminate while it is still on the cardboard or floor paper. Apply resin with brush or paint roller to all prepared areas of the joint. Lift all plies of glass together and, with the narrowest ply toward the inside, center the strap over the joint seam. Use an even, forward pressure to wrap around the joint, overlapping offset ends smoothly. With thick, large diameter
joints, it is often easier to apply this type strap in sections of half, or even one third, of the joint. Roll out, from the center to the edge of the strap, blending the edges into the pipe and removing all wrinkles and entrapped air. Care must be taken to prevent the joint laminate from sagging at the bottom of the pipe during the curing process.
13. Allow the EXTERIOR OVERLAY to cure and then do the INSIDE OVERLAY, if one is to be provided, using the same process as described above. Typically, the EXTERIOR OVERLAYS of several joints are made while previously overlaid joints are curing, before coming back and applying the INSIDE OVERLAYS. Note that the C-veil is applied last on an INSIDE OVERLAY so that it is the layer in contact with the corrosive liquid.
14. Sand off any rough edges before applying the final exterior coat, then mix the exterior wax coat resin. If supplied by FIBREX, this material will have an ultraviolet stabilizer in it as well as the paraffin wax. Apply this resin liberally to the exterior of the joint and inside overlay as well as all sanded areas for maximum corrosion and weathering resistance.


## LAYER SEQUENCE

| Contact Molded <br> Pipe Wall Thickness | 0.19 | 0.24 | 0.30 | 0.35 | 0.41 | 0.46 | 0.52 | 0.57 | 0.63 | 0.68 | 0.74 | 0.85 | 1.07 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

corrosion barrier (veil is 10 mil C glass, mat is $1-1 / 2$ oz. per sq. ft. )

| 6 " wide $C$-veil | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 " wide mat | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ | $2-3$ |

structural wall (mat is $3 / 4 \mathrm{oz}$. per sq. ft. except final layer of $1-1 / 2$ oz per sq. ft., woven roving is 24 oz per sq. yd.)

| 4" wide roving | 2 | 2 | 2 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 | 2-4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 " wide mat | 1-3 | 1-3 | 1-3 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 | 1-3-5 |
| 6 " wide roving |  | 4 | 4 | 6 | 6 | 6 | 6 | 6 | 6 | $6-8$ | $6-8$ | 6-8 | $6-8$ | 6-8 |
| 8 " wide mat |  | 5 | 5 | 7 | 7 | 7 | 7 | 7 | 7 | 7-9 | 7-9 | 7-9 | 7-9 | 7-9 |
| 8" wide roving |  |  | 6 | 8 | 8 | 8 | 8 | 8 | 8 | 10 | 10 | 10-12 | 10-12 | 10-12 |
| 10" wide mot |  |  | 7 | 9 | 9 | 9 | 9 | 9 | 9 | 11 | 11 | 11-13 | 11-13 | 11-13 |
| 10" wide roving |  |  |  |  | 10 | 10 | 10 | 10 | 10 | 12 | 12 | 14 | 14-16 | 14-16 |
| 12" wide mot |  |  |  |  | 11 | 11 | 11 | 11 | 11 | 13 | 13 | 15 | 15-17 | 15-17 |
| 12"wide roving |  |  |  |  |  | 12 | 12 | 12 | 12 | 14 | 14 | 16 | 18-20 | 18-20 |
| 14" wide mat |  |  |  |  |  | 13 | 13 | 13 | 13 | 15 | 15 | 17 | 19-21 | 19-21 |
| 14" wide roving |  |  |  |  |  |  | 14 | 14 | 14 | 16 | 16 | 18 | 22-24 | 22-24 |
| 16" wide mat |  |  |  |  |  |  | 15 | 15 | 15 | 17 | 17 | 19 | 23-25 | 23-25 |
| $16 "$ wide roving |  |  |  |  |  |  |  | 16 | 16 | 18 | 18 | 20 | 26 | 26-28 |
| 18" wide mat |  |  |  |  |  |  |  | 17 | 17 | 19 | 19 | 21 | 27 | 27-29 |
| 18" wide roving |  |  |  |  |  |  |  |  | 18 | 20 | 20 | 22 | 28 | 30-32 |
| 20" wide mat |  |  |  |  |  |  |  |  | 19 | 21 | 21 | 23 | 29 | 31-33 |
| 20 " wide roving |  |  |  |  |  |  |  |  |  |  | 22 | 24 | 30 | 34 |
| 22 " wide mat |  |  |  |  |  |  |  |  |  |  | 23 | 25 | 31 | 35 |
| 22 " wide roving |  |  |  |  |  |  |  |  |  |  |  | 26 | 32 | 36 |
| 24" wide mat |  |  |  |  |  |  |  |  |  |  |  | 27 | 33 | 37 |
| 24" wide roving |  |  |  |  |  |  |  |  |  |  |  | 34 | 38 | 38 |
| 26 " wide mat |  |  |  |  |  |  |  |  |  |  |  |  | 35 | 39 |
| $26 "$ wide roving |  |  |  |  |  |  |  |  |  |  |  |  |  | 40 |
| 28" wide mat |  |  |  |  |  |  |  |  |  |  |  |  |  | 41 |

NOTE: An experienced overlayer can apply several "stacked" layers of resin-saturated material at one time (see par. 12 of "Joining Procedures" on page 26). The number of layers depends on several factors including the diameter of the joint, required working time for roll-out and general site conditions. It is a good idea to start with 4-6 layers of mat and woven roving until the procedure can be assessed. Greater or fewer "stacked" layers can
then be applied, as required to attain maximum productivity while still allowing adequate time for proper roll-out of the laminate. In between applications of "stacked" layers, an exotherm, allowing the laminate to harden, is required.
$1-1 / 2$ oz. mat can be substituted for the $3 / 4 \mathrm{oz}$. mat but the same number of layers must be used. This will result in a thicker joint and will require approximately one third more resin.

## Shipping

IntegraLine pipe is shipped in one of the following ways:
Contract Truckload: Large orders are shipped by contract carrier on flatbed or stepdeck trailers. General dimensional restrictions for shipping pipe spools are $8^{\prime}-6$ " wide $\times 10^{\prime}-0$ " high ( $13^{\prime}-6$ " from road) $x$ up to $48^{\prime}-0$ " long
Common Carrier (LTL): Smaller orders, too big for UPS, are shipped LTL by common carrier. This type of shipment may be handled more than once during transit and will sometimes require special crating. It may also take longer to reach its destination than either contract trailers or UPS shipments.
UPS: Pipe components may be shipped via UPS with the following restrictions: Maximum weight per package: 150 LBS. Maximum Size per package: 108 inches in length, 130 inches in length and girth combined.
Contact your UPS Customer Service Office regarding availability of interstate service for packages weighing more than 70 pounds. The maximum weight for a Hazardous Materials package is 70 pounds unless further restricted in the UPS Guide for Shipping Ground and Air Hazardous Materials

## Measuring Your Package

(a) Measuring your packages for shipment by UPS involves length, which is longest side of the package, and girth, which is the distance around the widest part of the package at a right angle to the length.
(b) If the length plus the girth of a 3 Day Select, GroundTrac, or Ground package exceeds $84^{\prime \prime}$, contact your UPS Customer Service Office.
(c) If the length exceeds 108", the package is over UPS length limit and cannot be accepted.
(d) If the length plus the girth exceeds 130 ", the package is over UPS size limit and cannot be accepted.
Note: When figuring odd shaped components, girth is measured at the widest part. It is safest to picture the size box that would be required, even if it might not be shipped in one, and figure the girth and length on that basis.

## Handling and Storage

1. Caution should be used when handling FRP pipe and components to avoid any type of impact. FRP can be damaged internally (cracking and crazing) by abusive handling without exhibiting visible damage to the external surface.
2. When unloading or transporting pipe, each length, bundle (small diameter pipe) or spool should be handled individually. Do not unload by removing side stakes of trailer and allowing pipe to roll to the ground. Leave all plain end or flange protectors in place until pipe is to be installed.
3. When lifting the pipe by crane, a minimum of $3^{"}$ wide nylon slings should be used in conjunction with a spreader bar. Do not use chains or steel rope slings. Individual lengths of pipe can be lifted from one point if considerable care is exercised. Recommended practice for control and safety is that 20 ft . lengths of pipe should be lifted at two points, about 5 ft . from each end, and 40 ft . lengths should be lifted at two points about 10 ft . from each end.
4. Pipe stored for short term periods prior to installation should be stored on a flat surface free of any debris on which the pipe might inadvertently be placed.
5. Large diameter pipe stored for longer periods can be stacked by the use of saddle chocks. Chocks should be at least 3 " wide and 120 degrees of the pipe diameter. Pipes of like diameter may be stacked by using chocks both under and over the pipe to stabilize the sides and prevent ovaling. Saddle chocks should be no more than 10 ft . on center.
6. Small diameter pipe, and large diameter pipe not being stacked, may be stored by placing directly on 6 " wide racks or bearing boards. It is suggested that all pipe be supported on no more than 10 ft . spans with excess overhang divided equally between each end.
7. All field joint kits, resins and curing agents should be stored in a cool, dry place. DERAKANE resins should be stored between 50 and 75 degrees $F$., out of direct sunlight and away from all heat sources that might create localized hot spots on the resin container.

## UPS Shipment Limitations


$a+b+c+d=$ girth
L = length
Maximum length $=108^{"}$
Maximum length and girth $=130^{\prime \prime}$

Notes:

The information in this manual is derived from industry sources in addition to engineering design specific to the products described. There are many years of successful service of FRP pipe upon which the information and recommendations contained herein are based, but FRP pipe must be selected, installed and used in accordance with proven industry practice, common sense and sound judgment.

Further, the information contained in this manual must be considered as an expression of guidelines based on the sources and practices described above rather than a warranty for which Fibrex assumes responsibility. Fibrex offers separately, a limited warranty of its products, a copy of which is available upon request. In certain instances, Fibrex may provide direct engineering of a proposed installation or will assist in obtaining third party design engineering for specific projects that require it. The information contained in this manual cannot ensure, in itself, a successful installation and is offered to customers subject to these limitations and explanations.

Fibrex reserves the right, without notice, to change the specifications, design or other recommendations in this manual or other Fibrex literature without incurring any obligation for pipe or other equipment previously purchased from Fibrex. Information and descriptions contained in this manual are for the purpose of identification and neither limit nor extend the standard product limited warranty.


[^0]:    *Based on fluid contents specific gravity of 1.2

